



Microgrid Modeling Needs: Safety and Dynamic Interaction of Distributed Energy Resources

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Outline



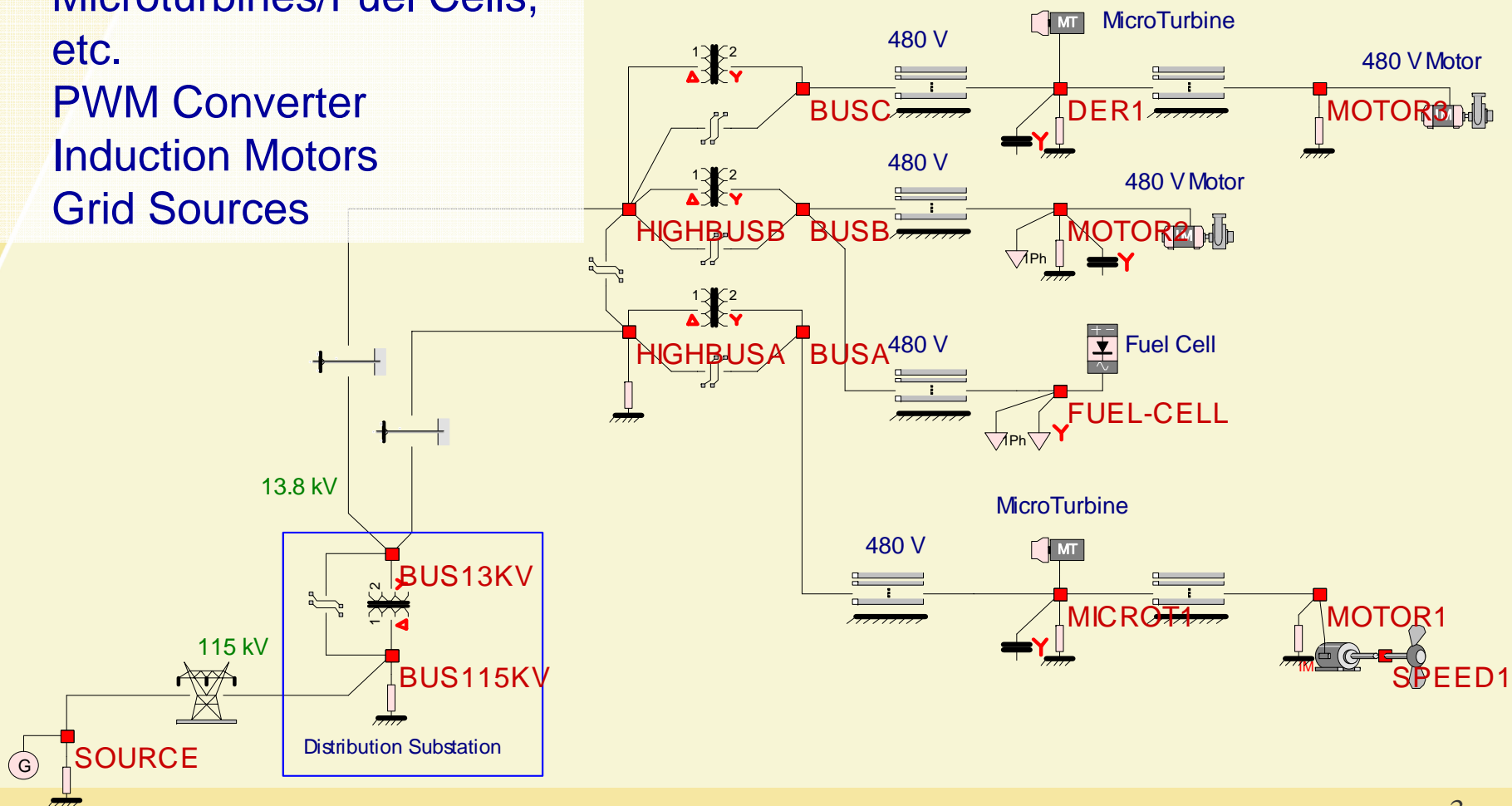
- Distributed Energy Systems - μ Grids
- Desirable Analytical Capability
- Modeling Methodology
- Safety Assessment – Stray Voltages
- Small Signal Stability Analysis
- Example Case Study
- Conclusions



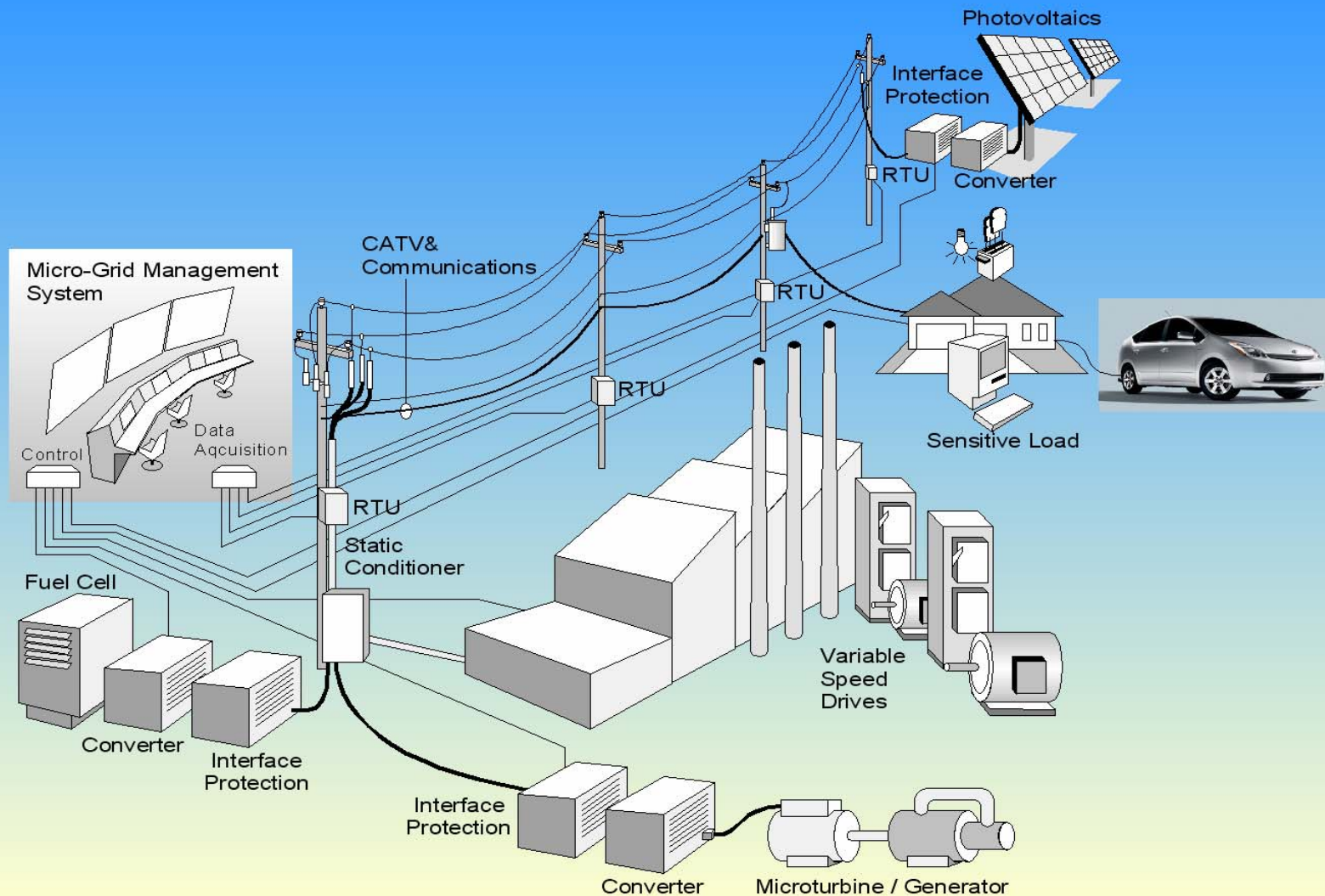
μGrids: Typical Configuration



- Power Lines
- Transformers
- Microturbines/Fuel Cells, etc.
- PWM Converter
- Induction Motors
- Grid Sources



The DER Concept for Utilities



Distributed Energy Resource Technologies



- Wind – Double Fed Induction Generators
- Photovoltaic
- Fuel Cells
- Microturbines
- Plug-In Hybrid Cars
- Storage: Batteries, Flywheels, Magnetic, etc.

Common Technical Characteristics

- Power Electronic Interface
- Inertialess
- Current Limited

Challenge and Opportunity



μ Grid Analysis Tool

Desirable Characteristics



- Analysis Tool for DER Integrated Systems That Captures all Physical Phenomena.
- The distribution system may contain three-wire, four-wire and five-wire circuits.
- The μ Grid may supply three phase as well as single phase loads.
- The μ Grid source (DERs) interface is via Inertialess Converters.
- The μ Grid sources may operate under different control laws. As a matter of fact, control functions are expected to increase as manufacturers become more sophisticated.
- A multiplicity of alternate operational philosophies.
- Interaction of Controls, Rating/Derating, Voltage Support at PCC, GenLoad-Frequency Control, Safety, etc.
- **Dynamic Interactions - Stability**



μ GRD: Unique Characteristics



- Components are modeled in **direct phase quantities** without any approximating assumptions, for example symmetrical components.
 - Provides the capability of handling three wire, four-wire and five-wire systems
 - Provides high fidelity models
 - Provides voltages and currents in Neutral wires and ground wires

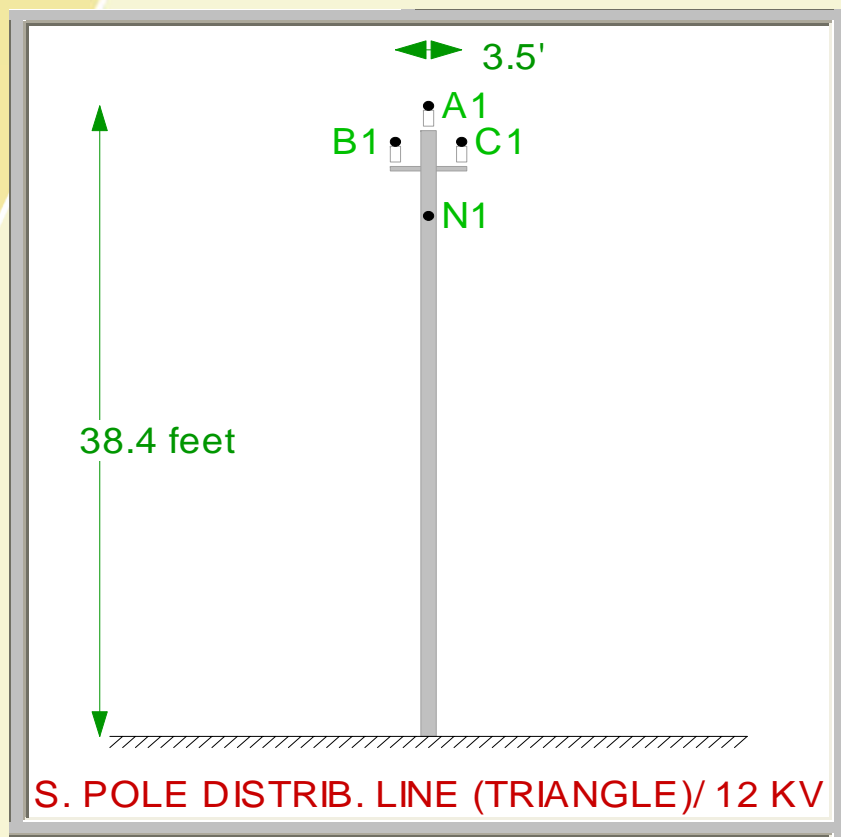


Direct Modeling: Physically Based Models



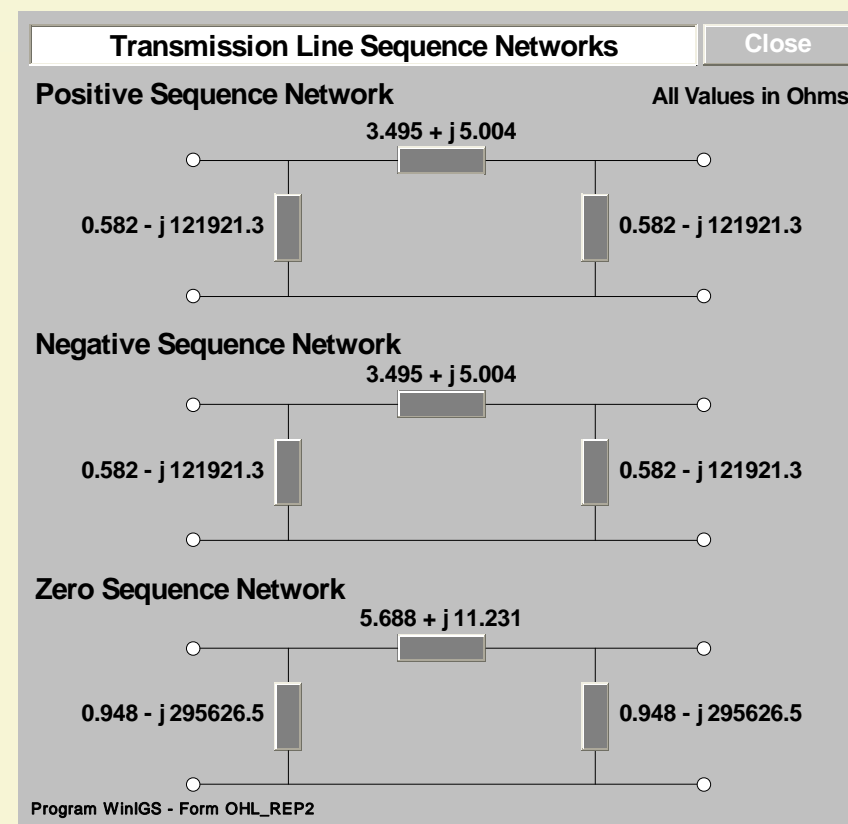
Example: **Three Phase Power Line**

Physically Based Model

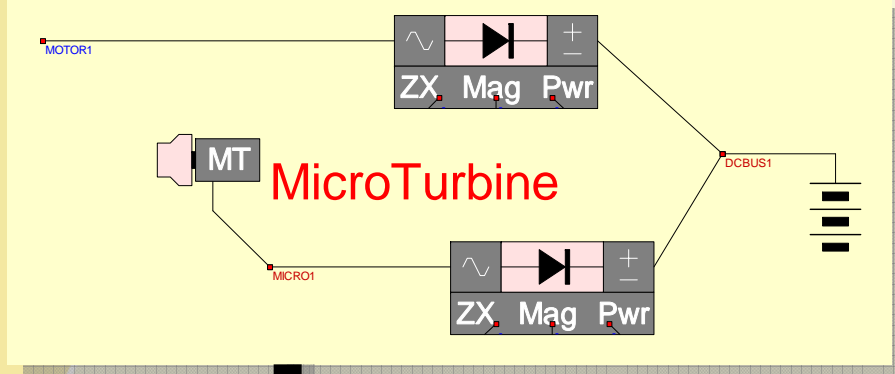


Sequence Parameter Model

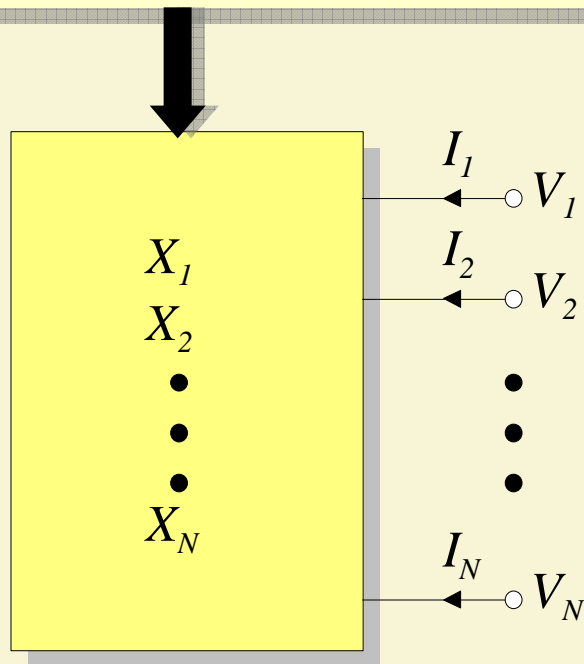
IT IS NOT USED



Quadratized Component Model



$$\begin{bmatrix} \dot{i}^k \\ 0 \end{bmatrix} = Y^k x^k + \begin{bmatrix} x^{kT} F_1^k x^k \\ x^{kT} F_2^k x \\ \vdots \end{bmatrix} - b^k$$



Where:

$$x^k = \begin{bmatrix} v^k \\ v^k \end{bmatrix}$$

**The model captures
any possible control
options**

**No
Simplifying
Assumptions**



Steady State Analysis



Component Model

$$\begin{bmatrix} I_r^k \\ I_i^k \\ 0 \end{bmatrix} = y_{eq_real}^k x^k + \begin{bmatrix} x^{kT} f_{eq_real1}^k x^k \\ x^{kT} f_{eq_real2}^k x^k \\ \vdots \end{bmatrix} - b_{eq_real}^k$$

Where

$$x^k = \begin{bmatrix} V_r^k \\ V_i^k \\ y^k \end{bmatrix}$$

Connectivity
Equations

System Model

$$G(x) = Y_{real} x + \begin{bmatrix} x^T f_1 x \\ x^T f_2 x \\ \vdots \end{bmatrix} - B_{real} = 0$$



Steady State Analysis



Component Model

$$\begin{bmatrix} I_r^k \\ I_i^k \\ 0 \end{bmatrix} = y_e^k$$

$$\begin{bmatrix} x^{kT} & f_{ea}^k & f_{real}^k \end{bmatrix} x^k$$

Solution - Newton's Method

Where

$$x^{v+1} = x^v - J_G^{-1} \left\{ Y_{real} x^v + \begin{bmatrix} x^{vT} f_1 x^v \\ x^{vT} f_2 x^v \\ \vdots \end{bmatrix} - B_{real} \right\}$$

$$G(x) = Y_{real} x + \begin{bmatrix} x^T f_2 x \\ \vdots \end{bmatrix} - B_{real} = 0$$



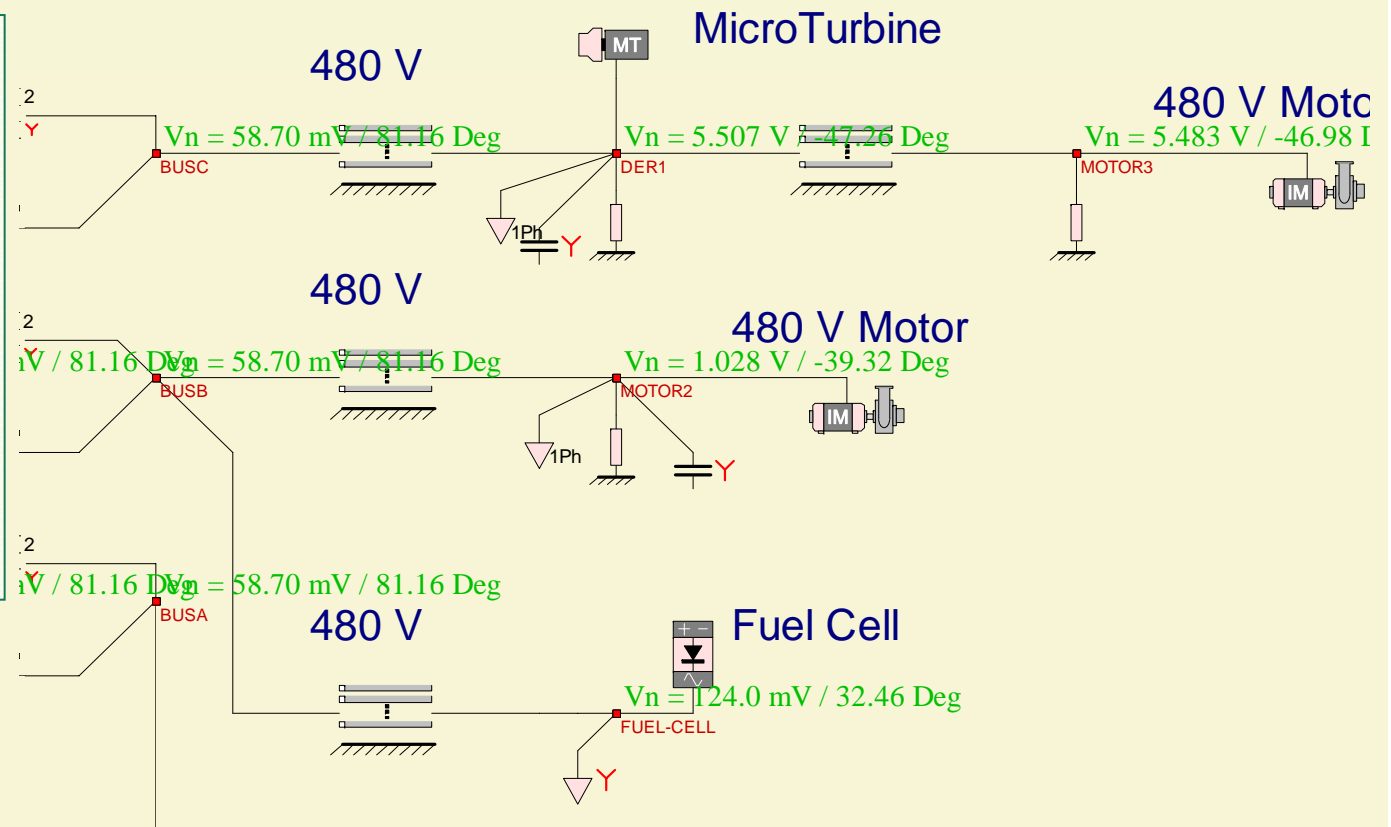
μ GRD Safety and Grounding



Exposure Factor:
More Folks Near a μ Grid versus an Electrical Installation

Safety Issues

- Touch Voltages
- Stray Voltages (Example)
- GPR
- Faults (in μ Grid and Utility)



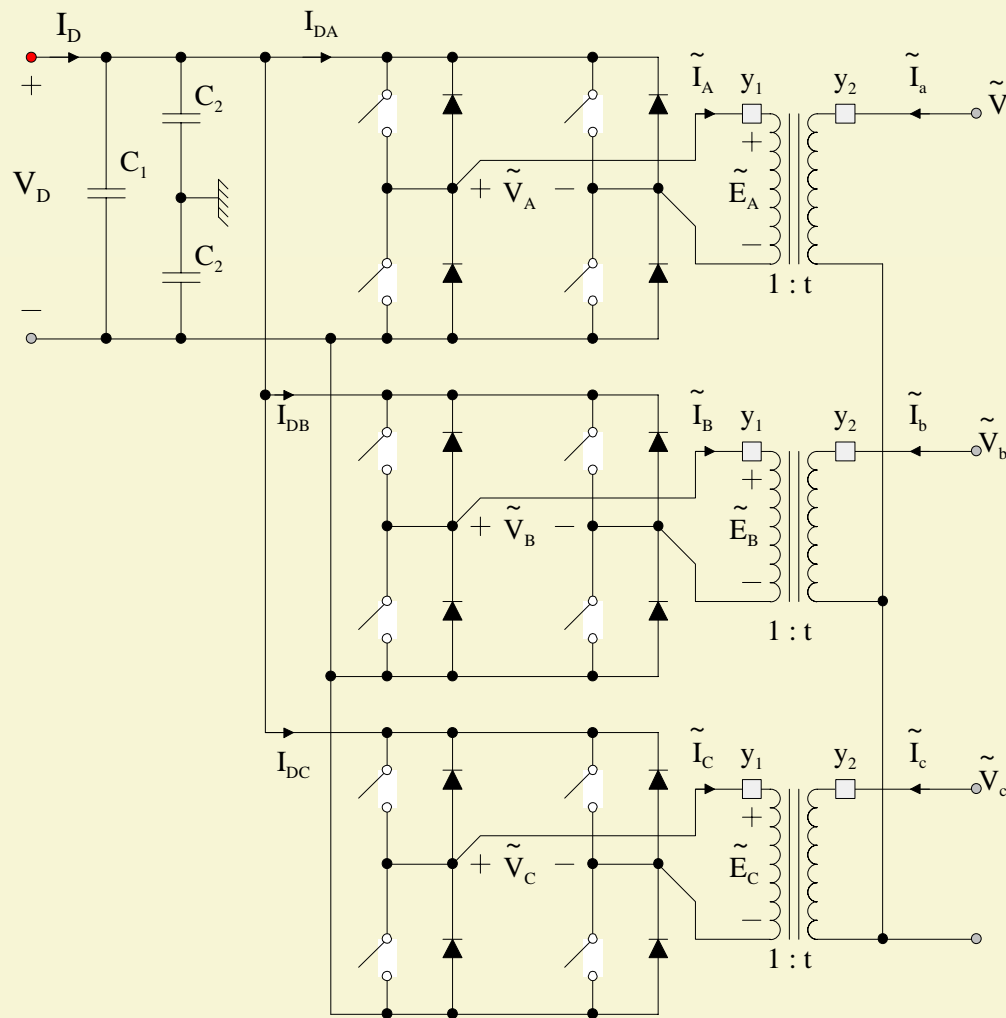
Interactions: Steady State, Dynamic, Stability



- DER Systems Have Their Own Controls
- DER Controls Interact Under Steady State Conditions (μ Grid Model)
- Multiple DERs on Same Circuit May Interact Dynamically
- New approach: Object Oriented Small Signal Stability



Microturbine-Utility Interface



Generic DC-AC
Converter with
Segregated
Phases



DC-AC Converter - Steady State Model



Interface Equations

$$\begin{cases} \tilde{I}_a = y_2 (\tilde{V}_a - t\tilde{E}_A) \\ \tilde{I}_b = y_2 (\tilde{V}_b - t\tilde{E}_B) \\ \tilde{I}_c = y_2 (\tilde{V}_c - t\tilde{E}_C) \\ I_d = I_A + I_B + I_C \end{cases}$$

Power Balance

$$\begin{cases} 0 = I_A^2 - y_1 y_1^* (\tilde{V}_A - \tilde{E}_A)(\tilde{V}_A - \tilde{E}_A)^* \\ 0 = I_B^2 - y_1 y_1^* (\tilde{V}_B - \tilde{E}_B)(\tilde{V}_B - \tilde{E}_B)^* \\ 0 = I_C^2 - y_1 y_1^* (\tilde{V}_C - \tilde{E}_C)(\tilde{V}_C - \tilde{E}_C)^* \end{cases}$$

Phase Control

$$\begin{cases} 0 = \tilde{V}_A - d\tilde{m}_a (x_1 + jx_2)V_d \\ 0 = \tilde{V}_B - d\tilde{a}^2\tilde{m}_a (x_1 + jx_2)V_d \\ 0 = \tilde{V}_C - d\tilde{a}\tilde{m}_a (x_1 + jx_2)V_d \\ 0 = x_1^2 + x_2^2 - 1.0 \end{cases}$$

Transformer

$$\begin{cases} 0 = y_2 t (\tilde{V}_a - t\tilde{E}_A) - y_1 (\tilde{V}_A - \tilde{E}_A) \\ 0 = y_2 t (\tilde{V}_b - t\tilde{E}_B) - y_1 (\tilde{V}_B - \tilde{E}_B) \\ 0 = y_2 t (\tilde{V}_c - t\tilde{E}_C) - y_1 (\tilde{V}_C - \tilde{E}_C) \end{cases}$$

DC Power

$$0 = V_d I_d - P_{\text{specified}}$$





Small Signal Stability - Eigenvalue Analysis

$$\frac{dx(t)}{dt} = Ax(t) \quad \leftrightarrow \quad x(t+h) = \Phi x(t)$$

$$\lambda_d \quad \leftrightarrow \quad e^{\lambda_a h}$$

λ_a *physical system eigenvalue – matrix A*

λ_d *discrete system eigenvalue – matrix Φ*

Small Signal Stability for μ Grids DERs Interfaced with Converters



Approach A:

Compute Transition Matrix,
Compute Eigenvalues of Transition Matrix

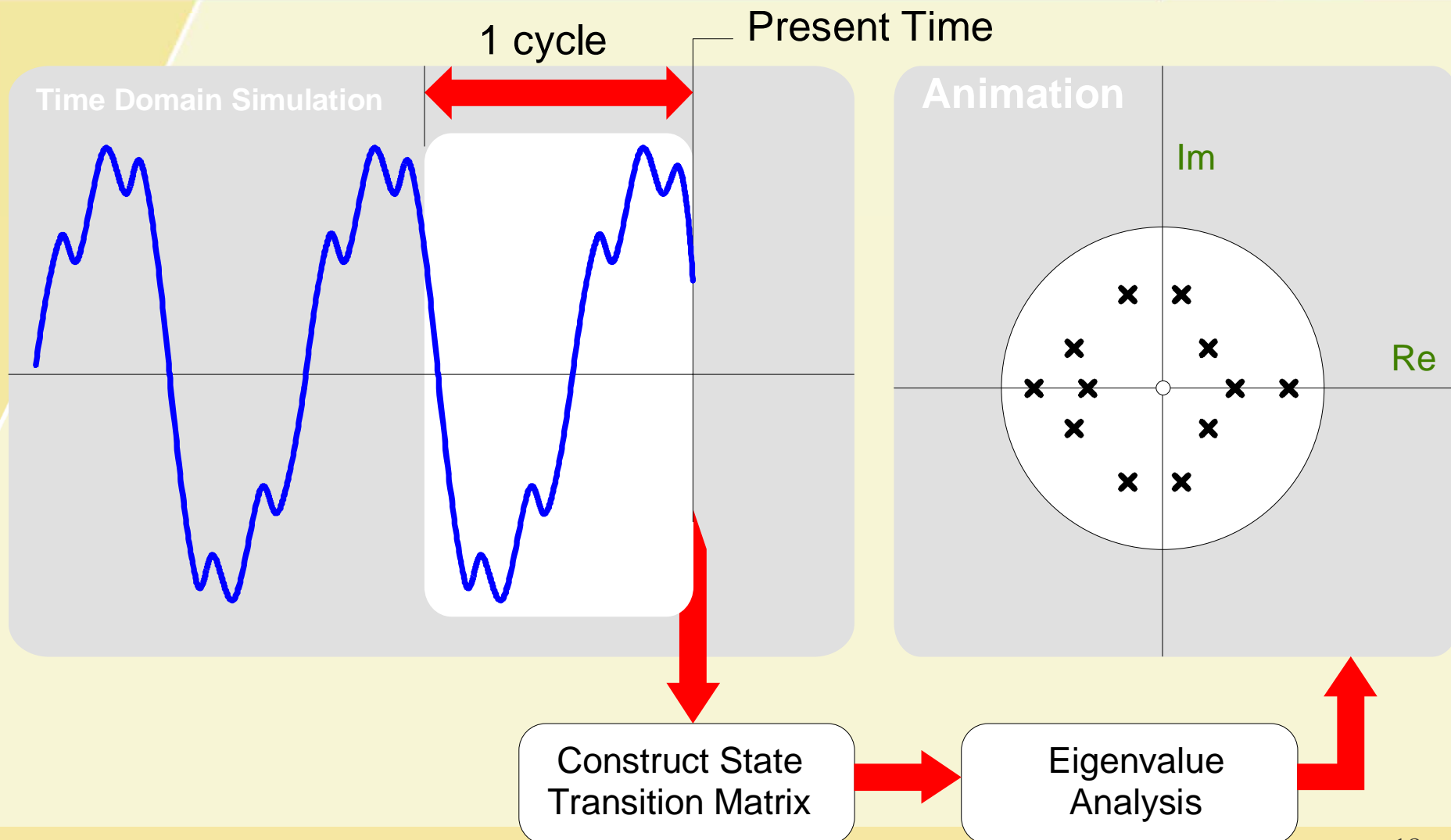
Approach B:

Derive Aggregate Quadratic Model,
Compute Steady State Solution
Linearize Model Around Solution
Compute Eigenvalues of Linearized Model

Validation: Compare Results



Small Signal Stability Analysis Approach B



Approach B



- Construct the Transition Matrix for Each Device
- Combine Device Transition Matrices into Network Transition Matrix
- Extract Eigenvalues of Network Transition Matrix



Stability Analysis Case Study

Case Description



Distribution System in Chesterton, Indiana



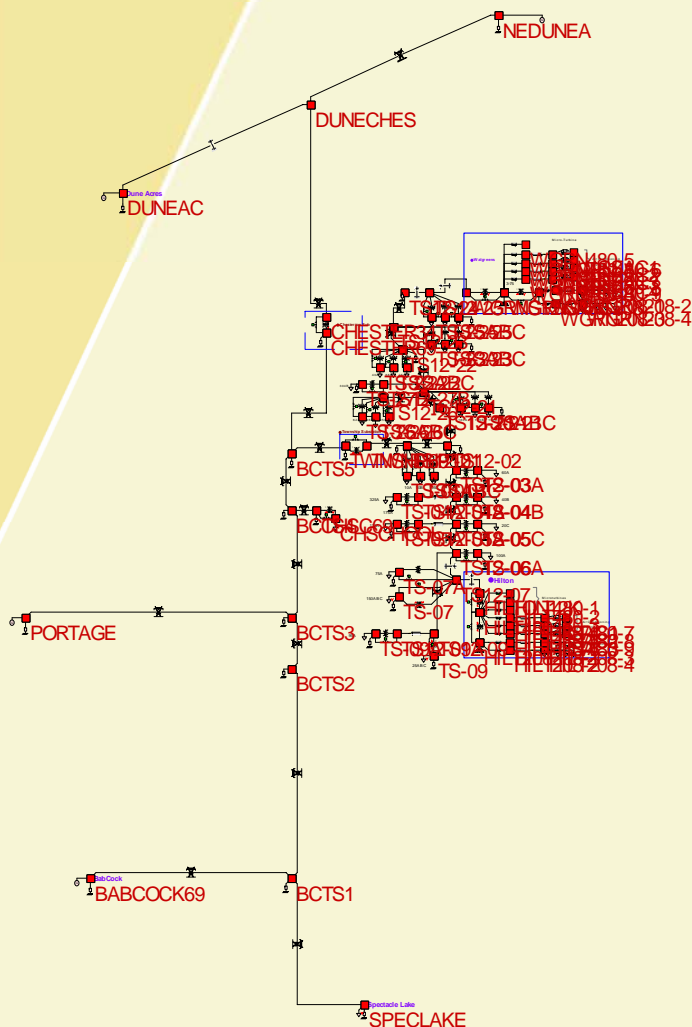
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Distribution System in Chesterton, Indiana



Model Includes:

- 12 kV Distribution System
- Four Distribution Substations
- 34 and 69 kV Transmission Lines Terminating at Substations
- Distribution Transformers and Major Loads
- **Four Microturbine DER's**



Stability Analysis Case Study

Case Descriptions

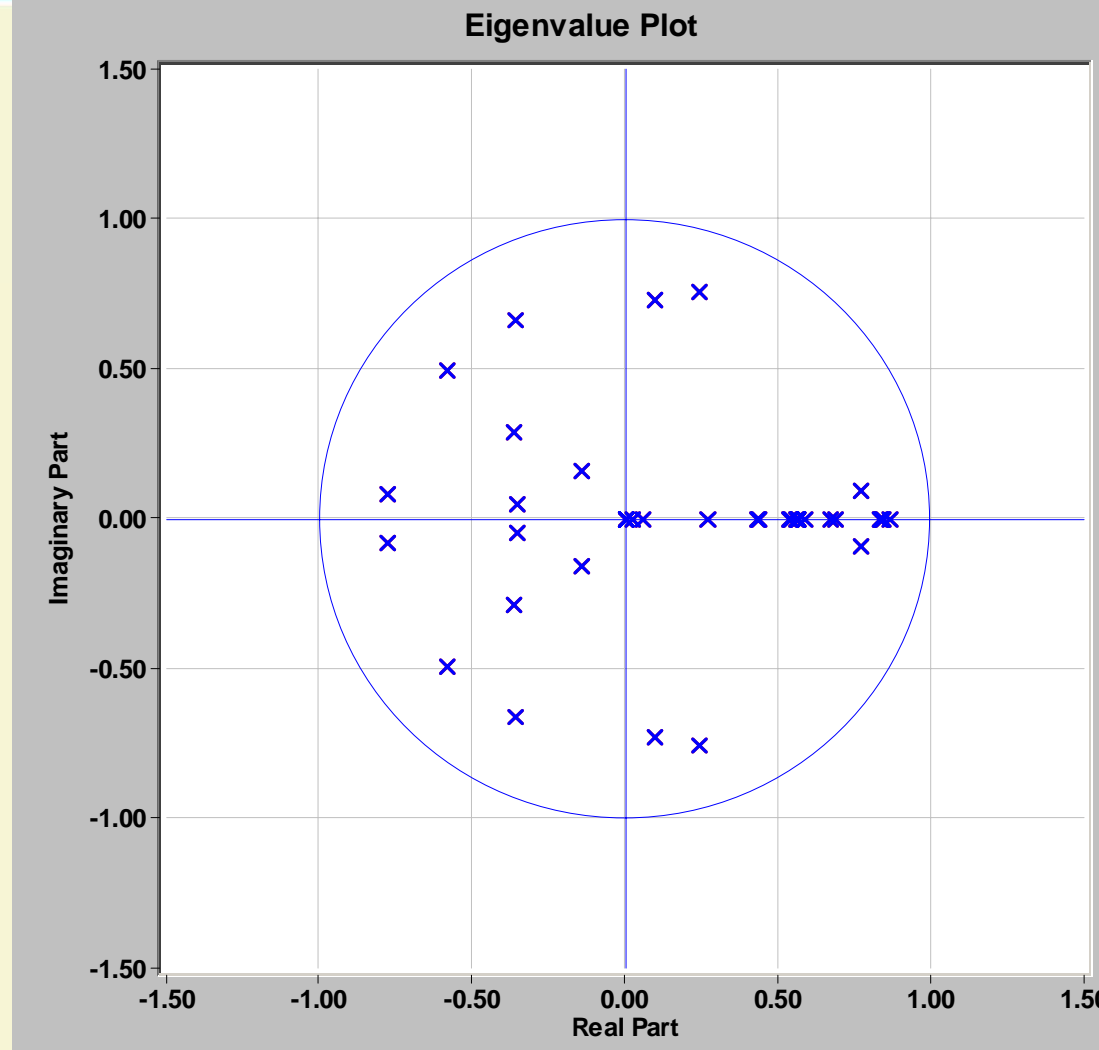


DER's Case #	DER#1	DER#2	DER#3	DER#4
Base Case	OFF	OFF	OFF	OFF
1	OFF	ON	OFF	OFF
2	ON	ON	OFF	OFF
3	OFF	ON	ON	OFF
4	ON	ON	ON	OFF
5	ON	ON	ON	ON
6	OFF	ON	ON	ON



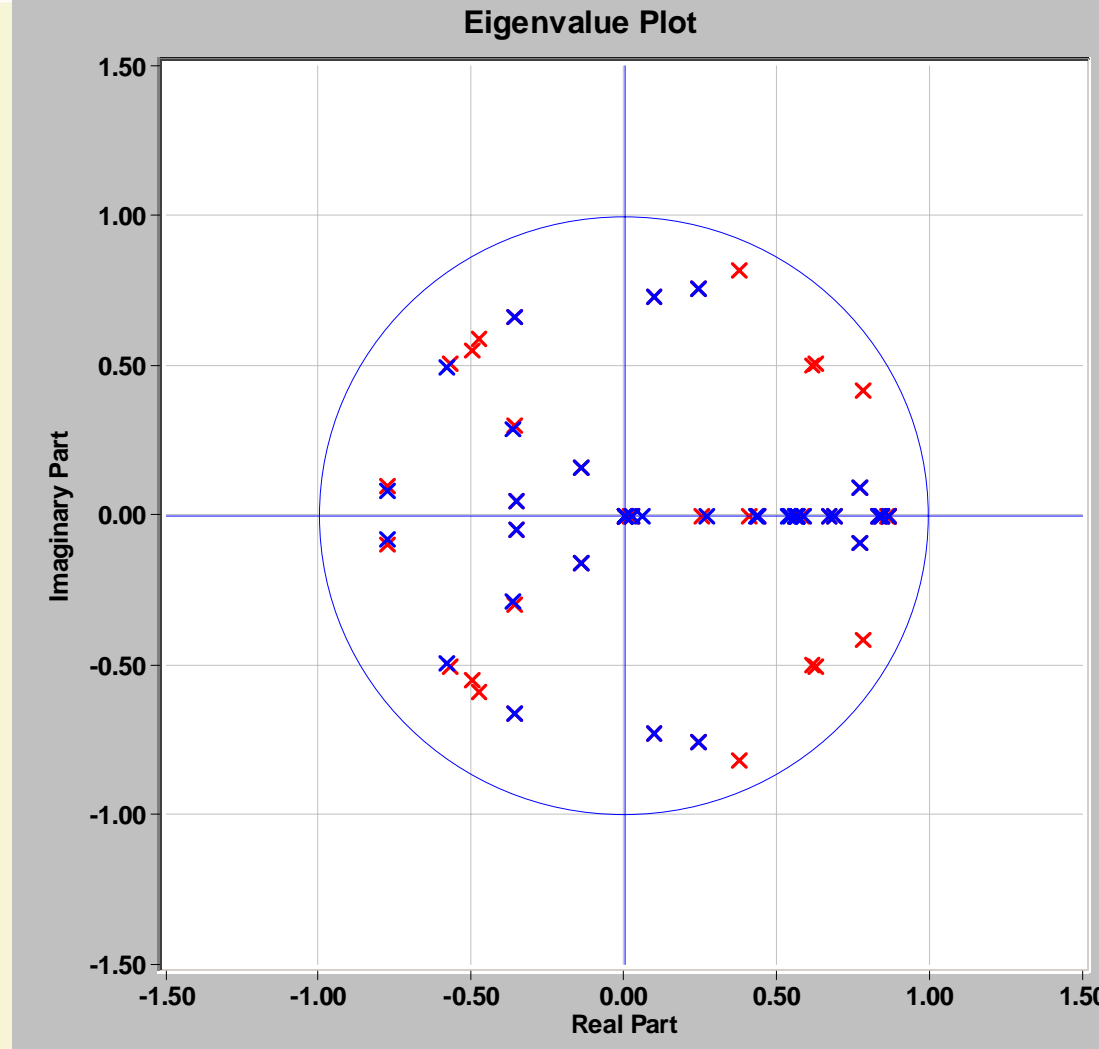
Stability Analysis Case Study

Base Case – Discrete System Eigenvalues



Stability Analysis Case Study

Case 2 – 2 DER'S ON – Discrete System Eigenvalues



Conclusions



- Understanding the dynamic interactions of μ Grids will lead to better designs of interfaces between the utility and the distributed energy resources.
- The feasibility of constructing an integrated model of the utility system and DER installations without any approximations was demonstrated. This model is useful in studying (a) safety issues, (b) protection issues and (c) the interaction of DERs with the utility system.
- The stability characterization of the integrated utility/distributed energy resources system exhibits dynamic interactions between utility/distributed energy resources as well as among distributed energy resources.
- The controls of the DER interface converter play a very important role in these dynamic interactions.
- Converter design and controls are usually proprietary. Cooperation with manufacturers to construct proper interface converters models will facilitate improved designs.



Τελος

